

F: magnetomotive force in ampere.turn
 N: number of turns
 I: current in amperes

1.2 MAGNETIZING FORCE

 The magnetizing force is defined as the magnetomotive force per unit length of path:

$$H=F/l \quad (2)$$

were:

H:magnetizing force in LENZ
 F:magnetomotive force in amper.turn
 l:length of path in cm.

1.3 PERMEABILITY

 The permeability (μ) is defined by the relationship:

$$\mu=B/H \quad (3)$$

were:

μ :Permeability
 B:Flux density, in GAUSS
 H:Magnetizing force in Lenz
 In the air, H is numerically equal to the flux density B

Permeability is the equivalent of conductivity in electrical circuits. Permeability in iron cores is not constant, but varies when the flux is varied. The relationship between B, H and μ is shown by the "BH characteristic curve" of the iron, as shown in FIG 2. and photos 2 and 3. The value of μ at any point is the value of B divided by the value of H at that point.

Generally the iron materials have high μ values, this implicates that the iron have high conductivity, or low resistance to the magnetic flux; iron is a good "magnetic conductor". In the opposite side, the air have low conductivity, and hence high resistance; air is a bad "magnetic conductor".

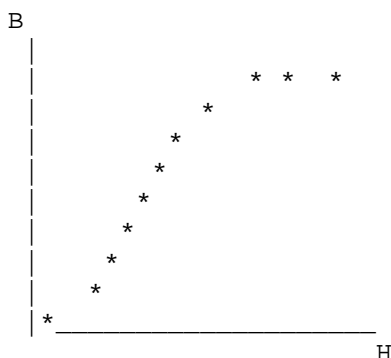


FIG 2. BH characteristic plot of iron.

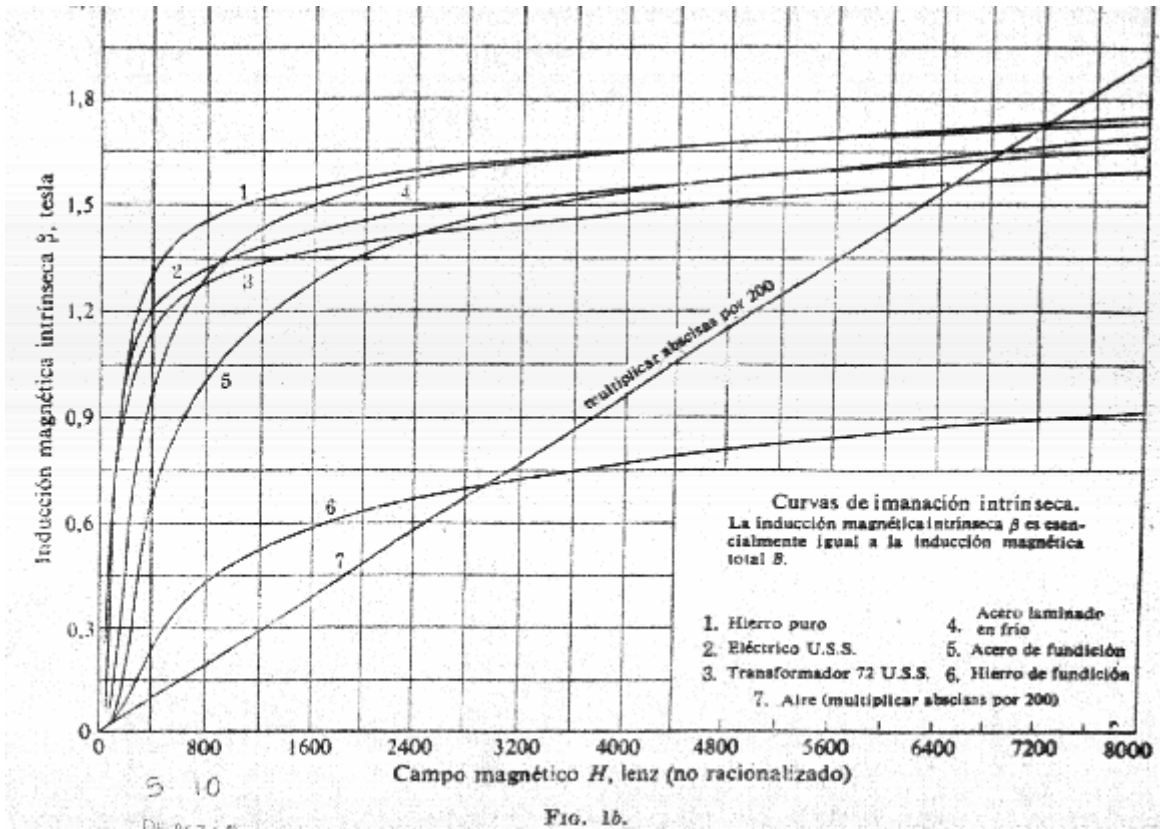


Photo 2.- B-

H iron curves

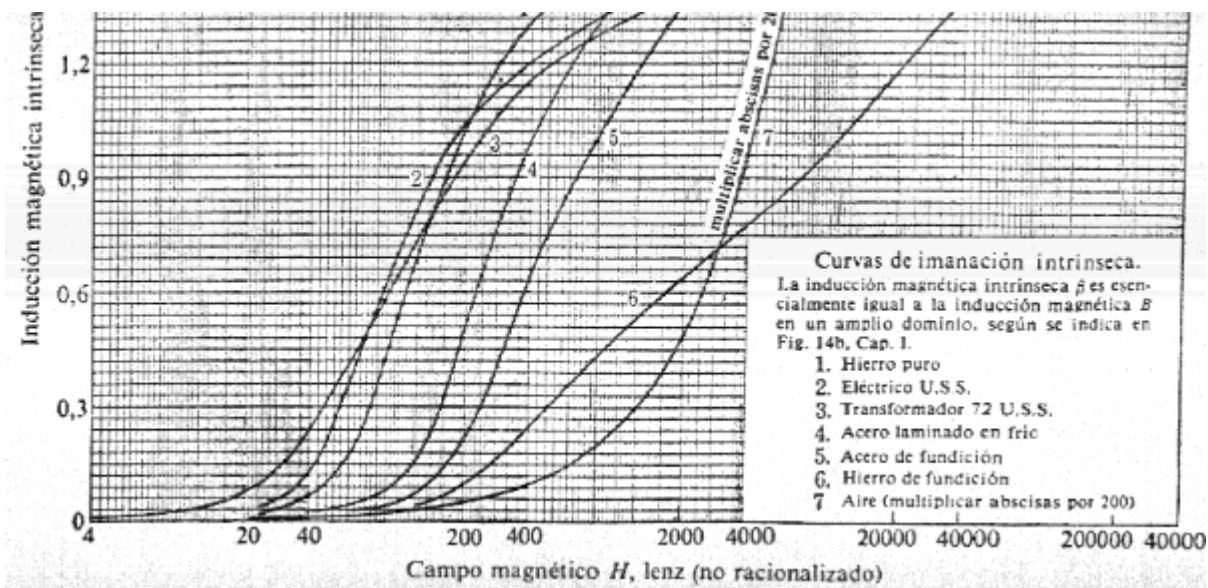


Photo 3.-

B-H iron curves, detailed for low H

2- PRACTICAL ELECTROMAGNET FOR EXAMPLES

Electromagnet to generate a field strength of 1174 gauss in a gap of 2 cm.

The square section of the iron is 5 x 5 cm.

The coil of the magnet have 720 turns of 1.5 mm wire. The coil length

is 12 cm.

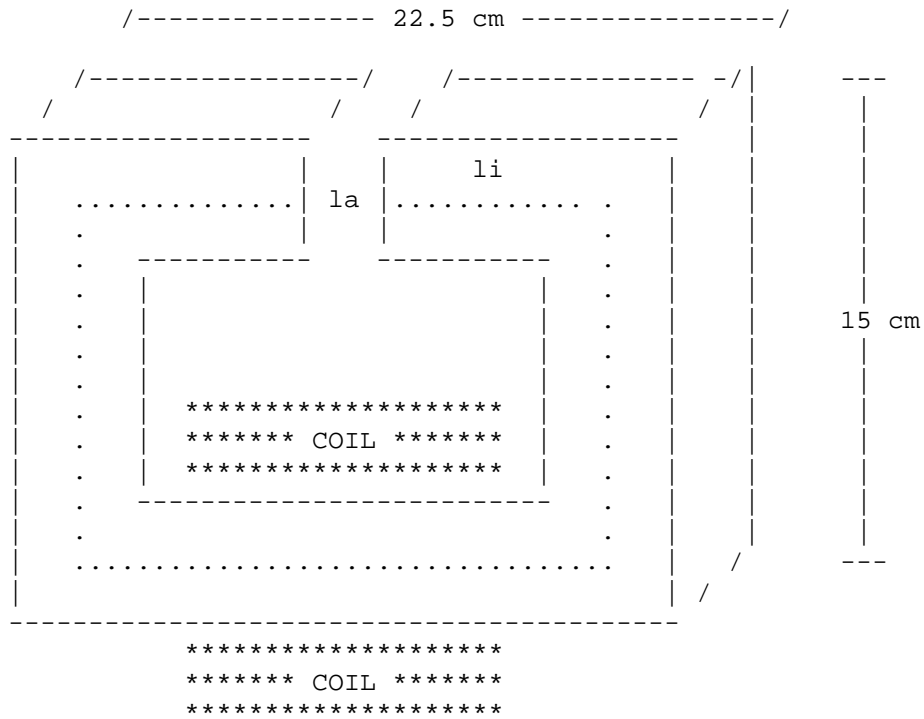


FIG 3. Physical dimensions of a practical electromagnet used for the examples. this was my first electromagnet I buid.

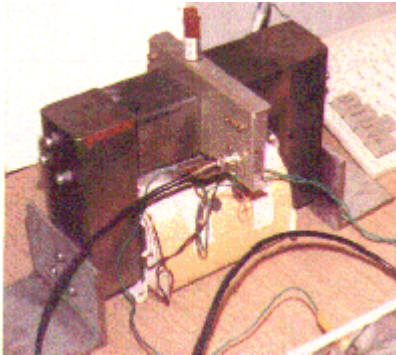
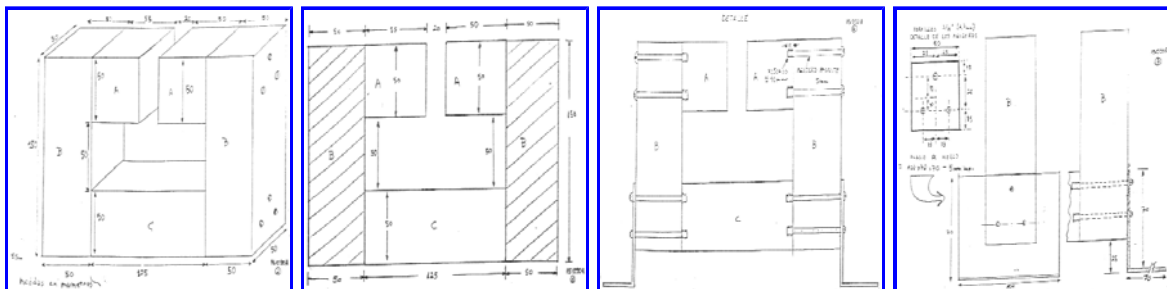


Photo 1.- First electromagnet for NMR experiments, show with probehead in the air-gap



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schematics of the electromagnet showing construction details

3-GENERAL CONSIDERATIONS

The following assumptions are generally made for simple theoretical treatment of circuit of FIG 1:

- 3.1 In the magnetic circuit, we assume that all necessary magnetomotive force is generated to overcome the air-gap "resistance".
- 3.2 The flux is confined itself entirely to the iron over the whole length of the iron path.
- 3.3 That the flux is uniformly distributed over the cross-sectional area of the iron.
- 3.4 That the iron area is the same along the magnetic circuit.
- 3.5 That the air gap length is small compared to the poles area.
- 3.6 That the gap area is the same as the iron area.

4- PRACTICAL DESIGN by BRUTE-FORCE method

Target:

Find the NI (ampere.turn) necessary to generate a desired flux density (B) in a determined air gap (la).

Solution:

In the magnetic circuit of FIG 1 we can assume that in the gap region, the magnetic induction is uniform, then:

$$H=B \quad (4)$$

H expressed in ampere.turn/cm

B expressed in gauss

Then we can assume that all magnetomotive force is necessary to overcome the gap resistance:

of eq. (2): $H=F/la$

of eq. (4): $H=B$

Then: $B=F/la$

Finally: $F=B * la \quad (5)$

Remember: $F= (N * I) / 0.796$ from eq. (1)

Then (5)=(1)

$$B * la= (N * I) / 0.796$$

Finally $N * I= 0.796 * B * la \quad (6)$

were:

N * I: is in ampere.turn
 B: is in gauss
 la: is in centimeters

NOTE: This BRUTE-FORCE method do not involve the dimensions of the magnetic circuit, except the AIR-GAP length.
However, as a first approximation have good results between +/- 10 %.

5- PRACTICAL CIRCUIT using the BRUTE-FORCE method.

Example:

For the NMR experiments, is needed a B of 1174 gauss in an air gap of 2 cm.

Then, the NI necessary are:

from eq. (6):

$$N * I = 0.796 * B * l_a$$

replacing values:

$$N * I = 0.796 * 1174 * 2 = 1869$$

$$\text{-----}$$

$$N * I = 1869$$

$$\text{-----}$$

Then, if we have a coil with 1869 turns, there must circulate one ampere of current to generate the necessary field in the gap.

The design of the coil is out of this paper.

Having built the electromagnet, from the practical circuit, we have the following values measured:

magnetic field of 1174 gauss (measured with NMR signal)
coil of 720 turns
current of 2.76 amperes (measured with digital ammeter 3-1/2 digit)

$$\text{then } N * I = 720 * 2.78 = 2001.6$$

This experimental value is between +7% of the theoretical value.
Photo 1 shown the electromagnet.

6- PRACTICAL DESIGN by A REFINED METHOD

In this method, we use the dimensions of the iron circuit, and the B-H curves of the iron (photos 2 and 3).

Target:

Find the N*I necessary to generate a desired B in a determined air-gap.

Solution:

In the magnetic circuit of FIG. 1 we can assume that in the gap region the magnetic induction is uniform, then:

$$\text{from eq. (4)} \quad H=B$$

Then we can calculate the total magnetomotive force, including now the iron length:

$$F = H_a * l_a + H_i * l_i \quad (7)$$

from eq. (3)

$$H = B / \mu$$

Then replacing H:

$$F = (B_a / \mu_a) * l_a + (B_i / \mu_i) * l_i$$

The μ of air, $\mu_a=1$, then:

$$F = B_a * l_a + (B_i / \mu_i) * l_i$$

assuming $B_a=B_i$:

$$F = B * [l_a + (l_i / \mu_i)] \quad (8)$$

from eq. (1) $F = (N * I) / 0.796$

Then (1)=(8)

$$(N * I) / 0.796 = B * [l_a + (l_i / \mu_i)]$$

Finally:

$$\text{-----}$$

$$N * I = B * 0.796 * [l_a + (l_i / \mu_i)]$$

$$\text{-----}$$

The value of μ_i must be obtained from the B-H curves of the iron, Photo 2 and 3.

7- PRACTICAL CIRCUIT by the REFINED method.

Verification of the practical circuit:

From FIG 3:

$B=1174$ gauss

$l_a= 2$ cm

$l_i= 54$ cm

$\mu_i= 2730$ from the B-H curves, see photo 3.

For this example, for $B=1174$ correspond a H of 35 Lenz, which correspond to 0.43 Oersted, curve 2 of photo 3. (See at end the conversion tables between units).

These values obtained graphically, are approximated.

Then $\mu_i=1174/0.43=2730$

replacing values:

$$N * I = 1174 * 0.796 * [(2 + (54 / 2730))]$$

$$N * I = 934.50 * [2 + 0.01978]$$

$$\text{-----}$$

$$N * I = 1887.4$$

$$\text{-----}$$

Then the refined method results: $N * I = 1887$
remember the brute force results: $N * I = 1869$
and the practical measurement: $N * I = 2001$

This results (refined) is near the -7 % of the practical measurement.

As you can see, the "resistance" of the iron path is very low, as compared to the "resistance" of the air-gap. Then, all the necessary $N * I$ generate is employed to overcome the air-gap "resistance".

Then this results arises that since refined method is only a little more exact and the BRUTE-FORCE method is preferable, for most practical designs. Both methods give results below the practical measurements between 7-8%.

Conversion between electromagnetics units

Multiply	BY	To get
F in uem	10	F in ampere.turn
F in Gilbert	0.7958	F in ampere.turn
F in ampere.turn	1.257	F in Gilbert
H in Oersted	79.58	H in Lenz
H in Lenz	0.01257	H in Oersted
H in Oersted	2.02	H in ampere.turn/inch
H in ampere.turn/inch	0.495	H in Oersted
B in Gauss	0.0001	B in Tesla
B in Tesla	10000	B in Gauss
B in Gauss	1	B in Maxwells/sq.cm
B in Gauss	6.45	B in Maxwells/sq.inch
B in Tesla	1	B in Weber/sq.metre

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Circuitos Magneticos y Transformadores- EE Staff del M.I.T. , 1965
Editorial Reverte, Spain.

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FINAL NOTE;

This design of electromagnets, was totally secondary to my main work in NMR, and was made only because I do not had any electromagnet at the time I begin to experiment in low resolution NMR techniques.

Probably, someone with good background in physics or in electromagnet design can made some observation in this paper, it will be welcome.

Norberto Raggio's Electromagnet Design Cookbook
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